

# Multiscale Simulations of Materials and Structures

## Lecture 7. *Dislocation Dynamics*

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@ Centre des Matériaux (virtually)  
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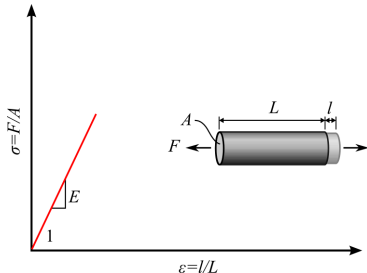
# Outline

- 1 Basics of dislocations
- 2 Notions in 2D
- 3 Extension to 3D
- 4 Burgers circuit
- 5 Dislocations motion
- 6 Stress field
- 7 Interaction of dislocations
- 8 DDD in 2&3D

# Introduction

## Notion of plasticity

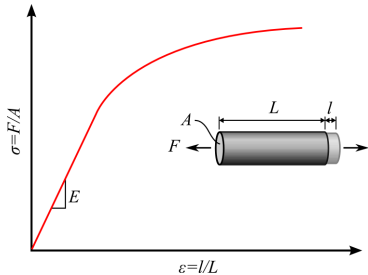
- Plasticity. . . irreversible change of shape
- In metals plasticity is the result of motion of linear defects of the crystal lattice: **dislocations**
- In rocks, for example, the plasticity is caused by slip at microcracks



Adapted from Wikipedia

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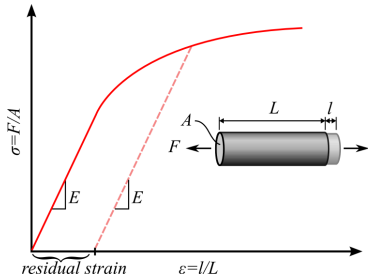


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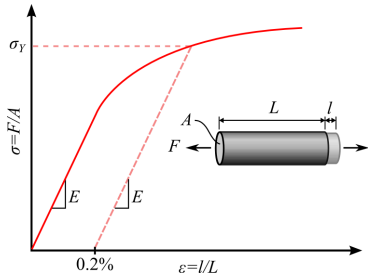


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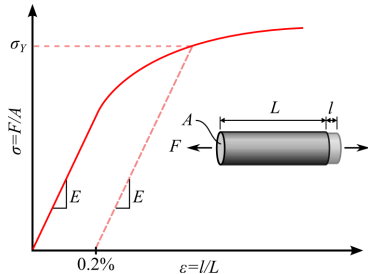


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# Introduction

## Notion of plasticity

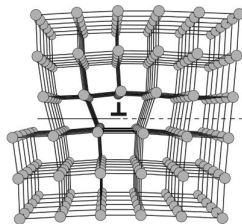
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## Objective:

- Understand basics of dislocation motion (*✓ for DMS students*)
- Convert this understanding into a computational model:  
**Dislocation Dynamics**

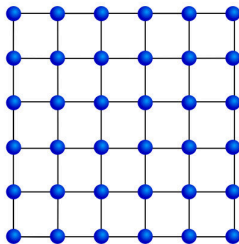


from

[1] Bulatov V.V., Cai W. Computer Simulations of Dislocations, Oxford University Press, 2006.

# Basic concept

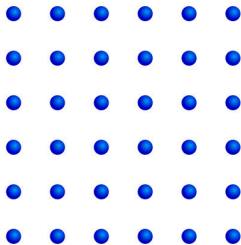
- Dislocation is a line defect, a curve in a volume
- But the basics can be understood in 2D...



Square lattice

# Basic concept

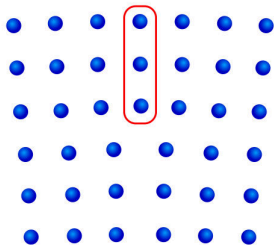
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Atoms arrangement

# Basic concept

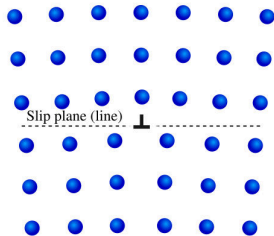
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Insert a half atomic layer  
(line in 2D, plane in 3D)

# Basic concept

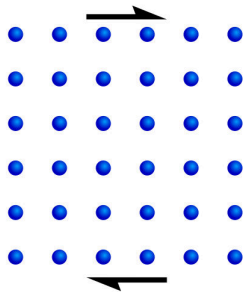
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Obtain a dislocation defect

# Basic concept

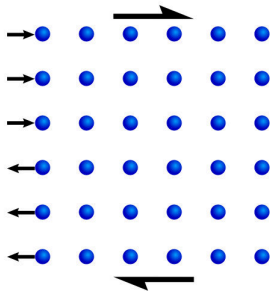
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Another option: let's shear this lattice

# Basic concept

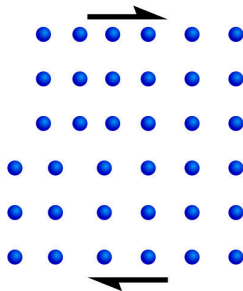
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or rather push and pull along a particular plane

# Basic concept

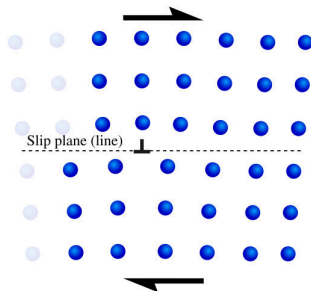
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Shift (make a step on left side)

# Basic concept

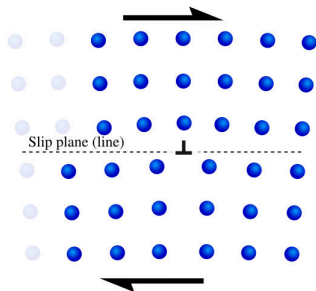
- Dislocation is a line defect, a curve in a volume
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Of course the lattice deforms accordingly,  
we can also imagine that we are far from free surfaces  
(add transparent atoms)

# Basic concept

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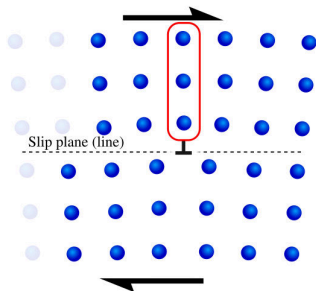


Let's shear more

or we might keep the same shear and wait until thermal fluctuations of atoms make the dislocation to step one step further

# Basic concept

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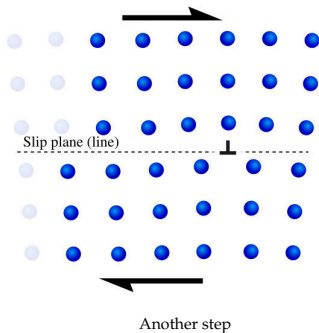


It has just make one more step

The configuration is equivalent as if we introduced a half  
atomic layer

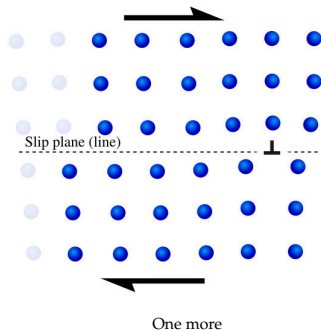
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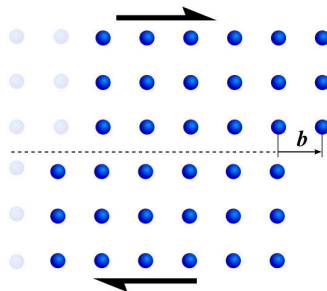
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# Basic concept

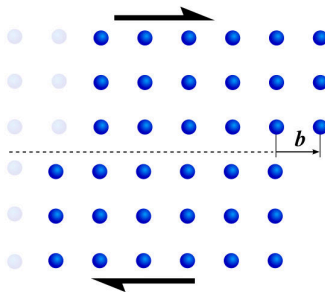
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One more, and there is no more dislocations... but if we remove shear, an irreversible deformation remains in the system

# Basic concept

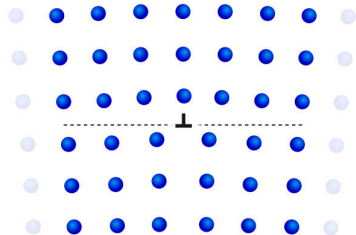
- Dislocation is a line defect, a curve in a volume
- But the basics can be understood in 2D
- Carpet fold analogy



One more, and there is no more dislocations... but if we remove shear, an irreversible deformation remains in the system

# Dislocation in 2D: Peierls potential

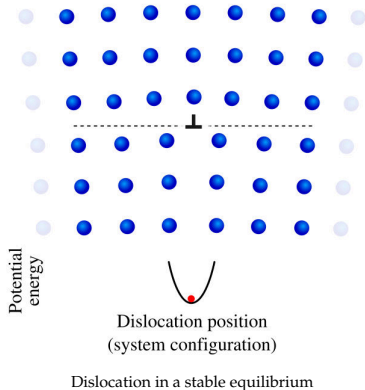
- Basics can be understood in 2D
- Concept of an array of potential wells and energy barriers



Dislocation

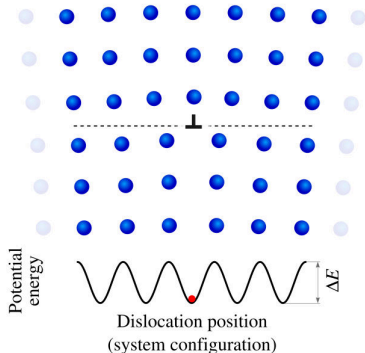
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# Dislocation in 2D: Peierls potential

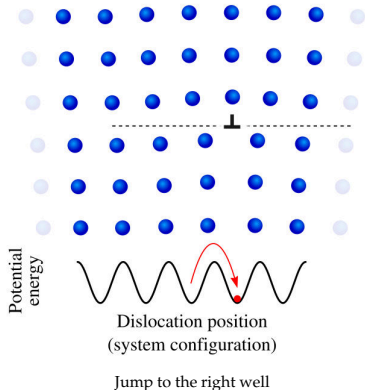
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Array of potential wells and energy barriers

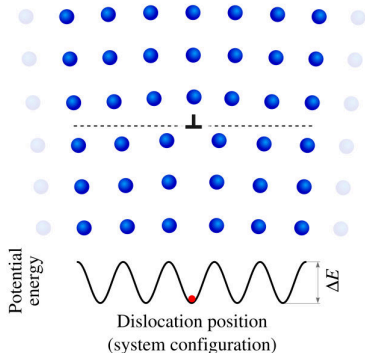
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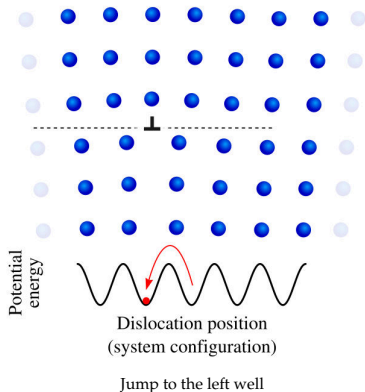
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Array of potential wells and energy barriers (**Peierls potential**)

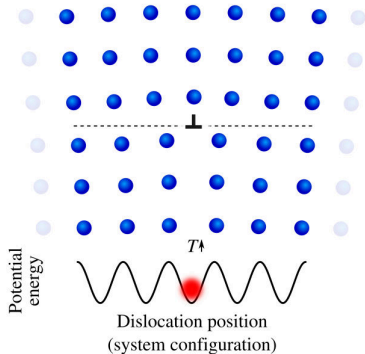
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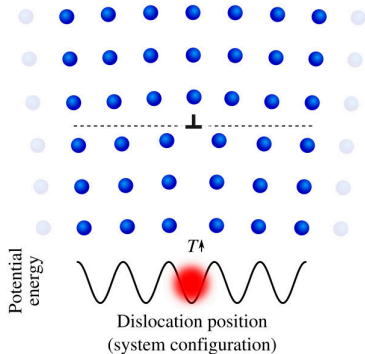
- Basics can be understood in 2D
- Concept of an array of potential wells and energy barriers
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- Thermally activated motion



Increasing temperature  $k_B T$  increases the probability of jump

# Dislocation in 2D: Peierls potential

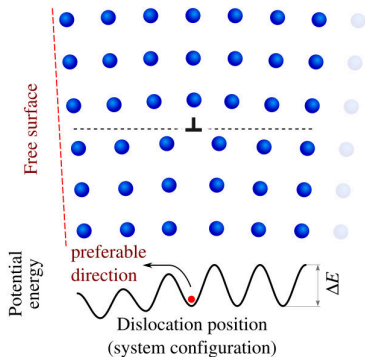
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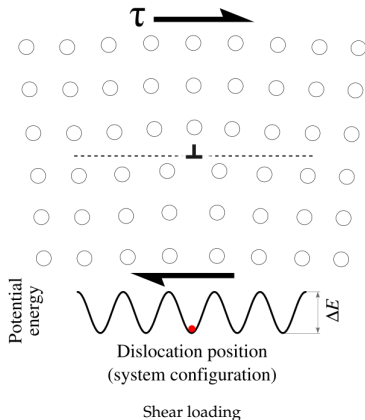
- Basics can be understood in 2D
- Concept of an array of potential wells and energy barriers
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- Thermally activated motion
- Interaction with free surface



Near the free surface, an energetically favorable direction of motion is towards the surface

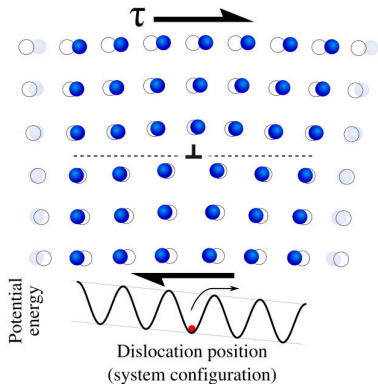
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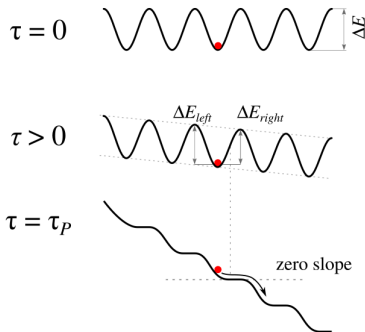
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Shear loading bias the potential and dictates the favorable direction of motion

# Dislocation in 2D: Peierls potential

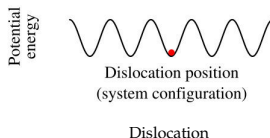
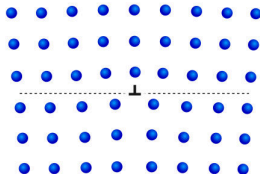
- Basics can be understood in 2D
- Concept of an array of potential wells and energy barriers
- Peierls potential
- Thermally activated motion
- Interaction with free surface
- Peierls stress



Increasing applied shear stress may result in a complete removing of the energy barrier (**Peierls stress  $\tau_P$** )

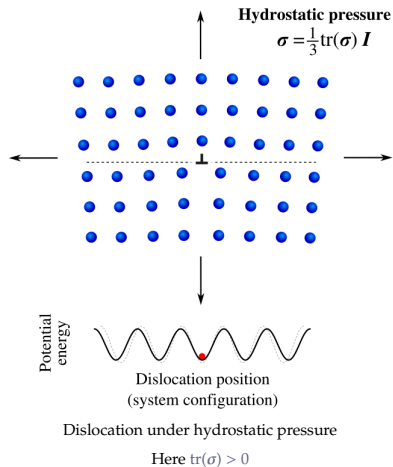
# Dislocation in 2D: stress effects

- Basics can be understood in 2D
- Applied stress affects dislocation motion



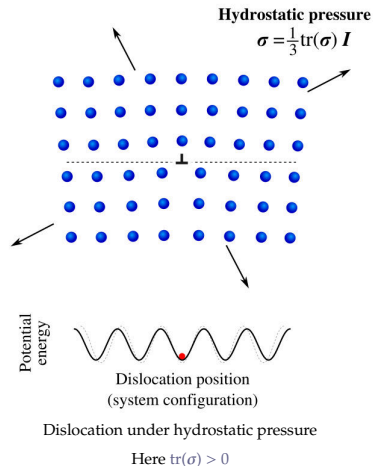
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- Basics can be understood in 2D
- Applied stress affects dislocation motion
- Rather insensitive to hydrostatic pressure



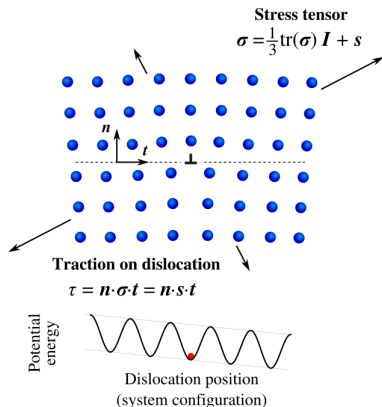
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- Sensitive to the stress deviator



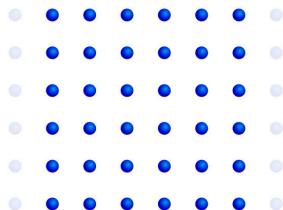
Dislocation is sensitive to the deviatoric part of the stress

$$s = \sigma - \frac{1}{3}\text{tr}(\sigma)I$$

$$\tau = n \cdot \sigma \cdot t = n \cdot s \cdot t$$

# Dislocation in 2D: stress effects

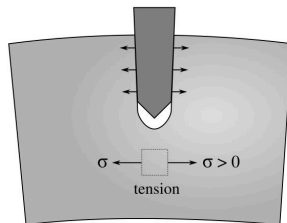
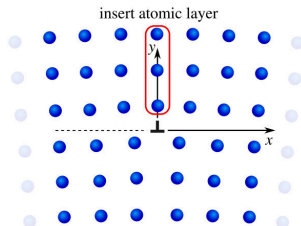
- **Basics can be understood in 2D**
- Applied stress affects dislocation motion
- Rather insensitive to hydrostatic pressure
- Sensitive to the stress deviator
- Dislocation itself induces stresses



Perfect crystal

# Dislocation in 2D: stress effects

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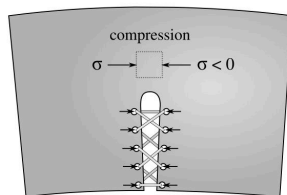
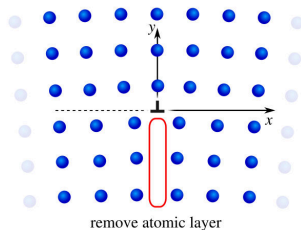


Dislocation: crystal with an **inserted layer** of atoms

Tensile stress below  $y < 0$ :  $\sigma_{xx} > 0$

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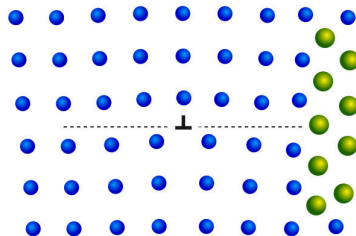
Dislocation: crystal with a **removed layer** of atoms

Compressive stress above  $y > 0$  :  $\sigma_{xx} < 0$

# Dislocation in 2D: stress effects

- **Basics can be understood in 2D**
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- Dislocation itself induces stresses
- Interactions with neighbouring defects: interstitial and vacancy defects

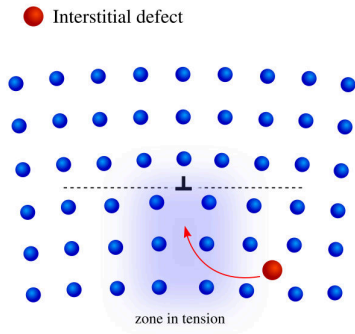
● Inclusion particle



Inclusion on the glide line

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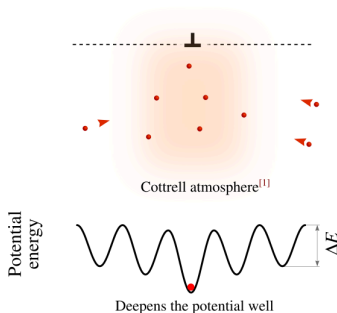


Interstitial defects migrate towards the zone of tensile stress induced by the dislocation

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● Interstitial defect

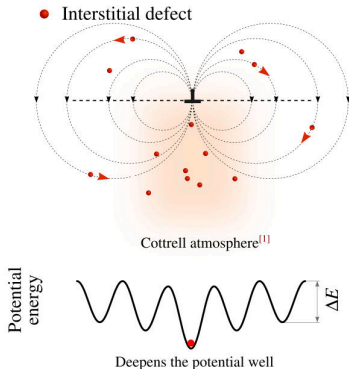


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[1] Cottrell & Bilby. Dislocation theory of yielding and strain ageing of iron. Proc Phys Soc A 62 (1949)

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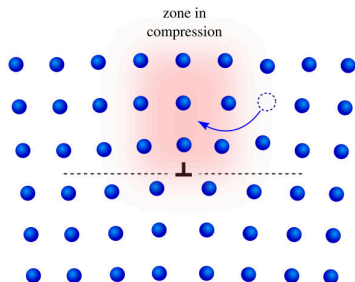


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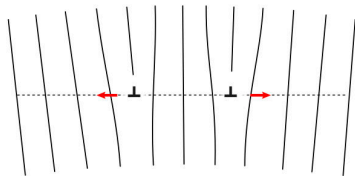
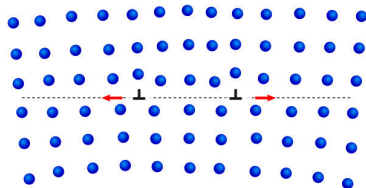


○ Vacancy defect

Vacancy defects migrate towards the zone of compressive stress induced by the dislocation

# Dislocation in 2D: stress effects

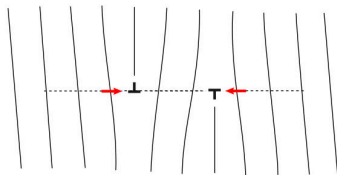
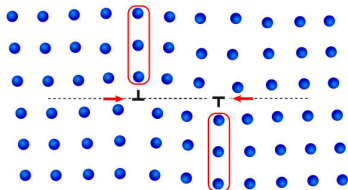
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- Interactions with neighbouring defects: interstitial and vacancy defects
- Interactions between dislocations



Interaction of two “up” dislocations is repulsive

# Dislocation in 2D: stress effects

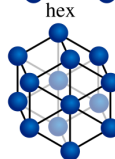
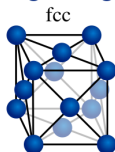
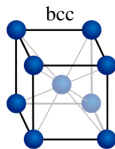
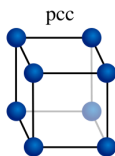
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Interaction of “up” and “down” dislocations is attractive  
and leads to annihilation of both defects

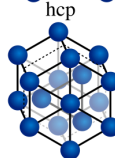
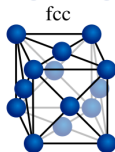
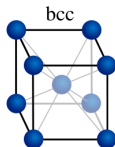
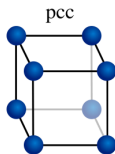
# 3D lattices

- Basics can be understood in 2D
- **But the complete picture can be drawn only in 3D**
- Crystallographic lattices in 3D:
  - primitive cubic (pcc)  
(very rare for pure metals, *Po*)
  - body-centered (bcc)  
(common, *Fe*, *Cr*, *W*, *Nb*)
  - face-centered cubic (fcc)  
(common, *Al*, *Cu*, *Au*, *Ag*)
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(common, *Be*, *Mg*, *Zn*, *Ti*)
- + and 10 other bravais lattices.
- Slip planes  $n = (ijk)$  (often the most densely packed)
- slip systems  $d = [prs]$  (often the most densely packed)  
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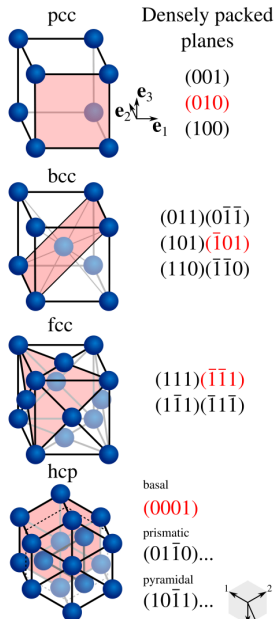
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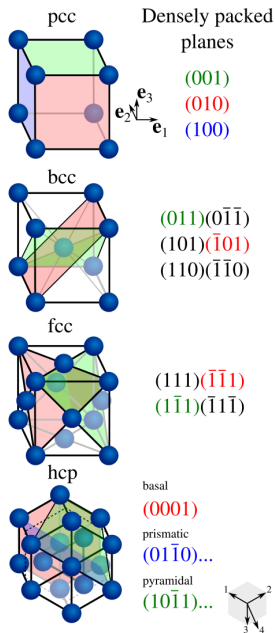
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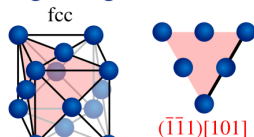
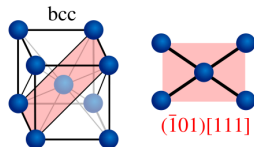
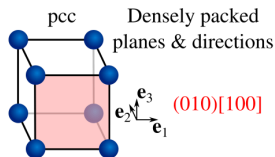
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# 3D lattices

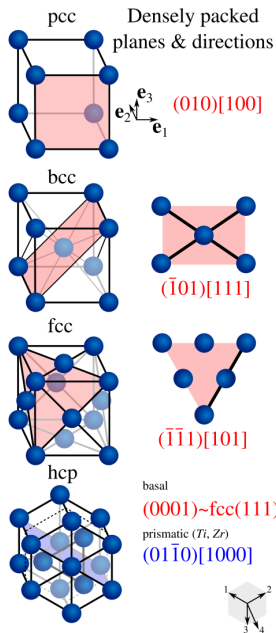
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# 3D lattices

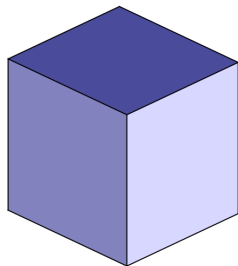
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# 3D dislocations

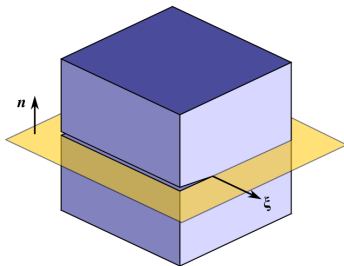
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Box

# 3D dislocations

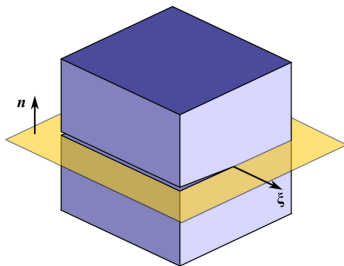
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Introduce a cut along a densely packed plane with normal  $n$  (e.g. (111) in fcc)

# 3D dislocations

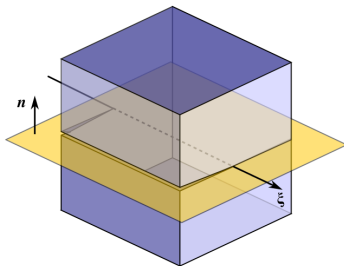
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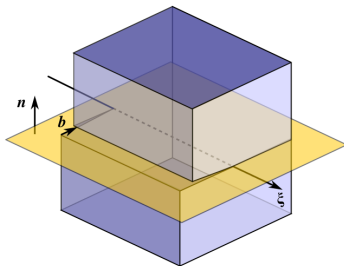
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Cut's edge is the dislocation line,  
introduce an orientation  $\xi$

# 3D dislocations

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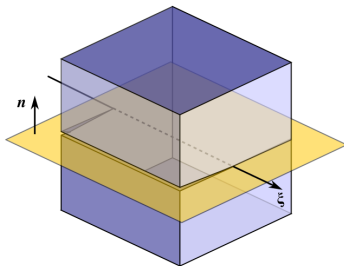


Shift the cut by a vector  $b$  along the plane **orthogonally** to the dislocation line and glue sides

**Edge dislocation**

# 3D dislocations

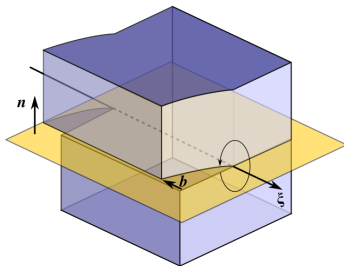
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Cut in the box

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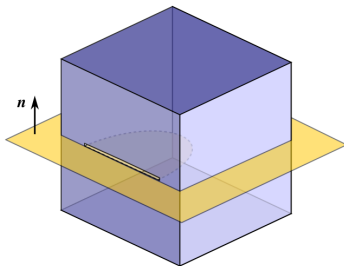


Shift the cut by a vector  $b$  along the plane **parallel** to the dislocation line and glue sides

**Screw dislocation**

# 3D dislocations

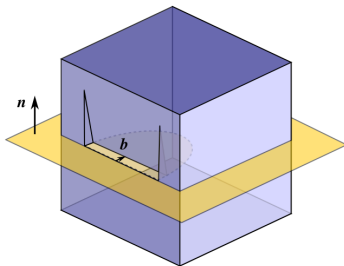
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Semi-circular cut in the box

# 3D dislocations

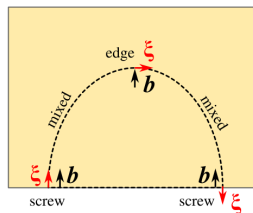
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Shift the cut by a vector  $b$  and obtain a complex dislocation combining **screw and edge** dislocations

# 3D dislocations

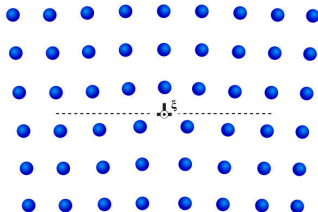
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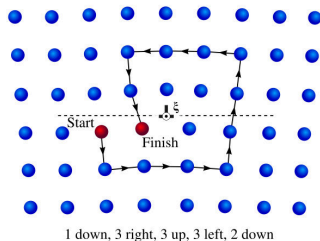
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Edge dislocation

# 3D dislocations

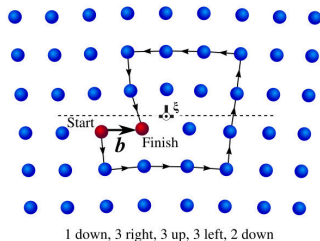
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Make a contour around  
(right-hand rule *la règle de la main droite*)

# 3D dislocations

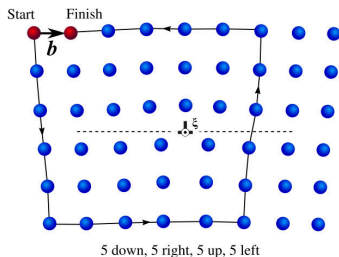
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Make a contour around  
(right-hand rule *la règle de la main droite*), compute the net Burgers vector

# 3D dislocations

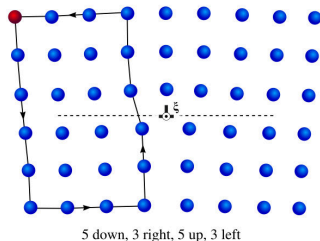
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Change the contour

# 3D dislocations

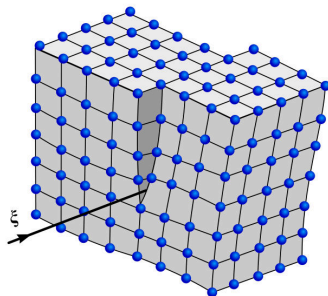
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Make a contour around a dislocation-free zone  $b = 0$

# 3D dislocations

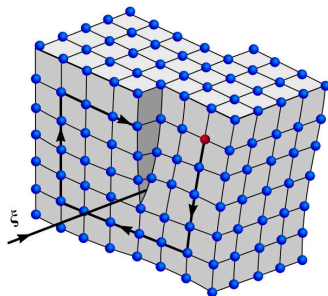
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Screw dislocation

# 3D dislocations

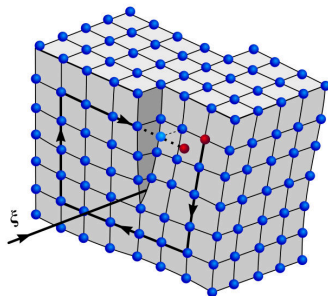
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Draw a contour:  
4 down, 5 left, 4 up, 3 right

# 3D dislocations

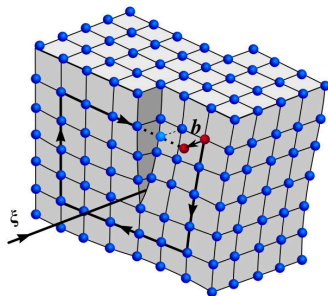
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Draw a contour:  
4 down, 5 left, 4 up, 3+2 right

# 3D dislocations

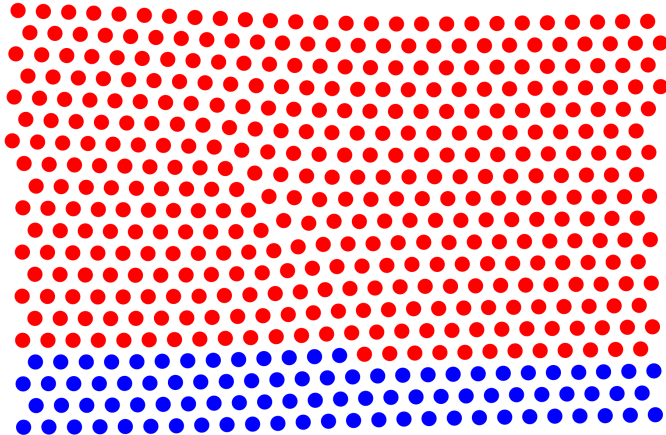
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The Burgers vector is collinear  
with the dislocation line  
 $b \parallel \xi$

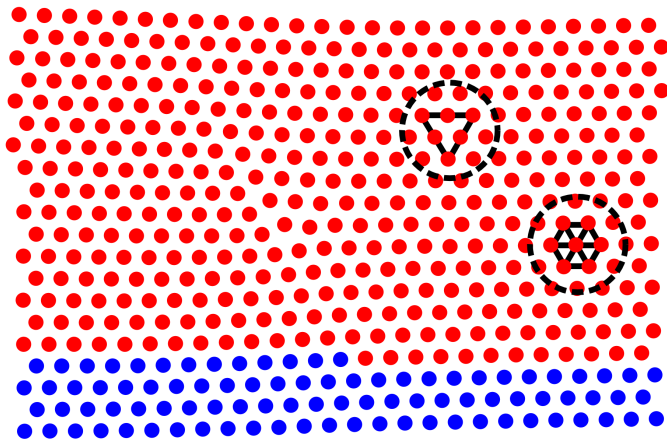
# Burgers curcuit example

*Example from the Monday lecture on Molecular dynamics*



# Burgers circuit example

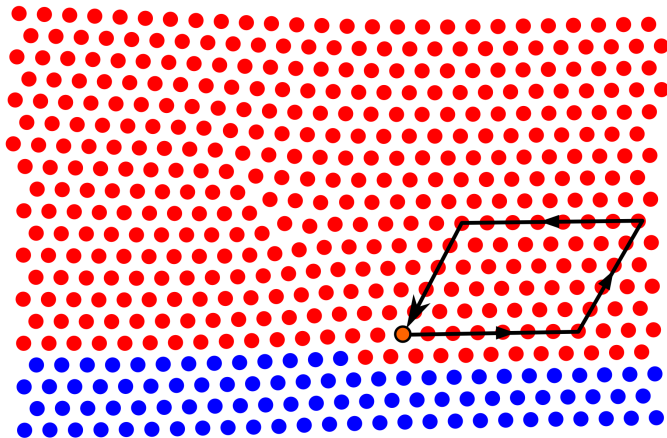
*Example from the Monday lecture on Molecular dynamics*



Basal hcp (0001) or fcc slip plane (111)

# Burgers circuit example

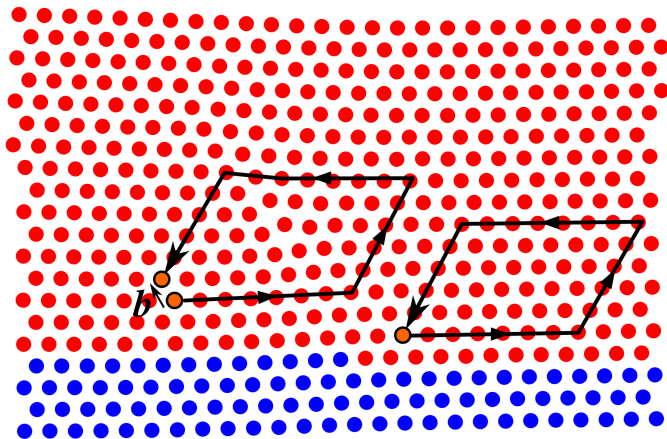
*Example from the Monday lecture on Molecular dynamics*



Contour 1:  $b = 0$

# Burgers circuit example

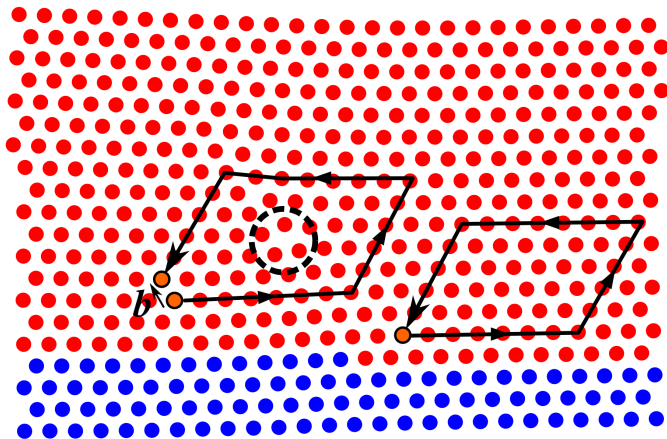
*Example from the Monday lecture on Molecular dynamics*



Contour 2:  $\mathbf{b} = \frac{a}{\sqrt{2}} [\bar{1}10]$

# Burgers circuit example

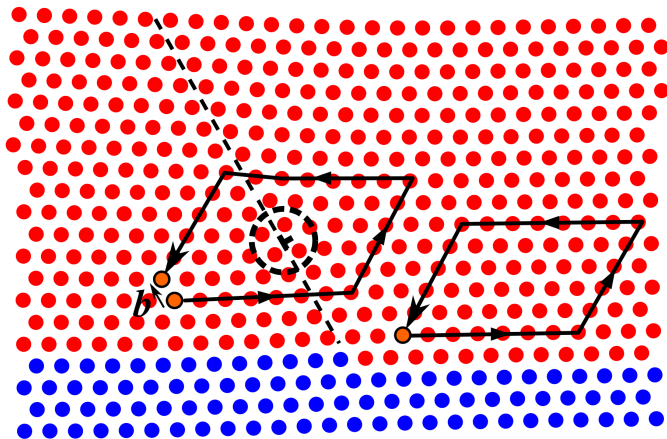
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Contour 2:  $b = \frac{a}{\sqrt{2}} [\bar{1}10]$

# Burgers circuit example

*Example from the Monday lecture on Molecular dynamics*



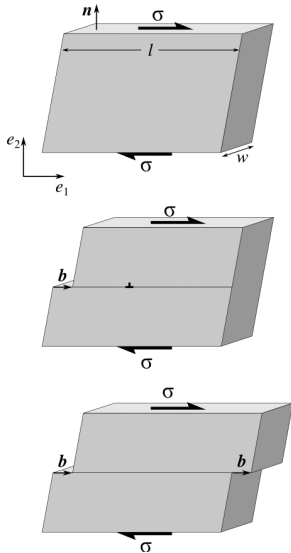
Contour 2:  $\mathbf{b} = \frac{a}{\sqrt{2}} [\bar{1}10]$

# Forces on dislocations

- A uniform stress  $\sigma$  shears a single crystal
- Force on the top  $f = \int \sigma \cdot n dA = \sigma_n w l$
- Work of this force on shearing the crystal by amount  $b = e_1 |b|$ :  
 $W = f \cdot b = w l \sigma_n \cdot b$
- At the same time dislocation of length  $w$  moves the distance  $l$
- The “virtual” force  $f$  acting on the dislocation makes the same work:  
 $w l f e_1 = W = w l \sigma_n \cdot b$  so  
 $f = (\sigma_n \cdot b) e_1$
- More generally (valid for edge and screw dislocations)

$$f = (\sigma \cdot b) \times \xi$$

(Peach-Koehler force)



# Forces on dislocations

- Example: Frank-Read source in (111) plane with  $b \sim [0\bar{1}1]$ , e.g.  $b = \frac{a}{2\sqrt{2}}(e_3 - e_1)$
- The box with this dislocation is under a uniaxial tension  $\sigma = \sigma e_3 \otimes e_3$
- Let's compute the Peach-Koehler force as

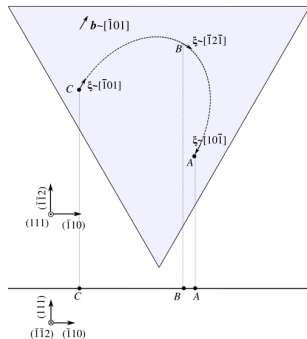
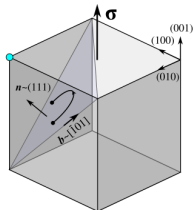
$$f = (\sigma \cdot b) \times \xi$$

- Where  $\sigma \cdot b = \sigma \frac{a}{2\sqrt{2}} e_3$

- At A:  $\xi = \frac{dl}{\sqrt{2}}(e_1 - e_3)$ ,  $df = \sigma \frac{a}{4} e_2 dl$

at B:  $\xi = \frac{dl}{\sqrt{2}}(2e_2 - e_1 - e_3)$ ,  $df = -\sigma \frac{a}{4}(e_1 + e_2) dl$

at C:  $\xi = \frac{dl}{\sqrt{2}}(e_3 - e_1)$ ,  $df = -\sigma \frac{a}{4} e_2 dl$



Note: line tension and self-interaction are not considered

# Forces on dislocations

- Example: Frank-Read source in (111) plane with  $b \sim [0\bar{1}1]$ , e.g.  $b = \frac{a}{2\sqrt{2}}(e_3 - e_1)$
- The box with this dislocation is under a uniaxial tension  $\sigma = \sigma e_3 \otimes e_3$
- Let's compute the Peach-Koehler force as

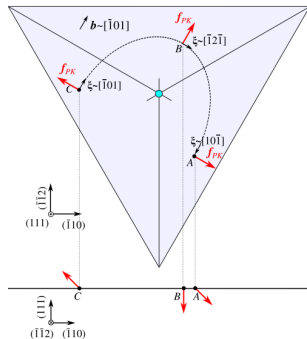
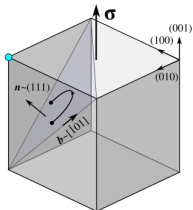
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Note: line tension and self-interaction are not considered

# Forces on dislocations

- Apart from the external load, dislocation has a **line tension** [J/m]
- Elastic energy per unit length stored around a dislocation (screw or edge)

$$E = \alpha \mu b^2, \quad \alpha \approx 0.5 - 1$$

- Line tension acting along the dislocation line is

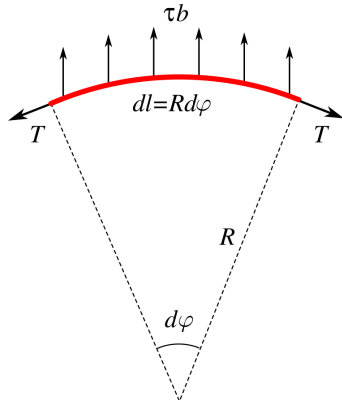
$$T = \alpha \mu b^2$$

- Then for a curved dislocation of radius  $R$ :

$$T d\phi = \tau b dl = \tau b R d\phi$$

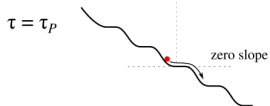
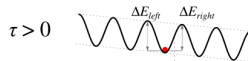
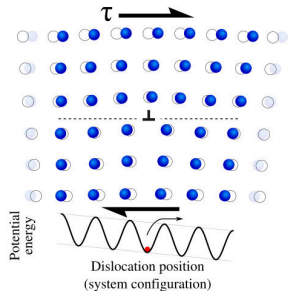
- For equilibrium (to keep this dislocation curved)

$$\tau = \alpha \mu b / R$$



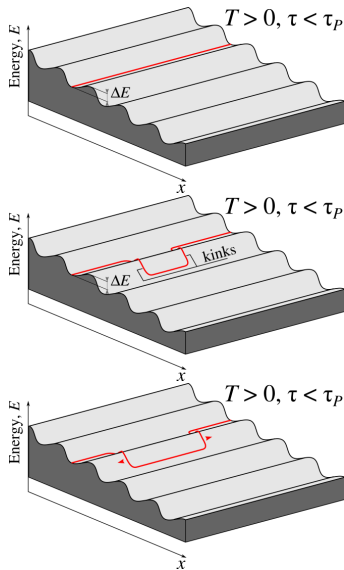
# Dislocation motion

- Recall the 2D case
- But dislocations are not point defect



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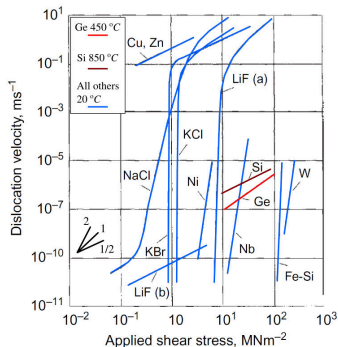


# Dislocation motion

- Recall the 2D case
- But dislocations are not point defect
- When the resolved shear  $\tau$  is smaller than the Peierls stress  $\tau_p$ , thermally activated motion propagate via **kinks**
- When  $\tau > \tau_p$ , dislocations glide in “viscous drag” regime, where dislocation velocity is proportional to the force as well as the lattice friction

$$v_{\text{dis}} \sim f_{PK}, \quad f_{fr} \sim -g(T)v_{\text{dis}}$$

- Friction force  $f_{fr}$  comes from thermal vibrations of the lattice (phonons)
- In FCC: often viscous drag regime
- In BCC: viscous drag for edge and kinks-mechanism for screw

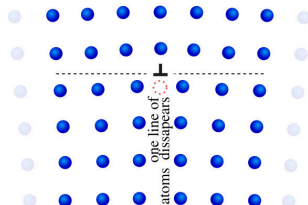
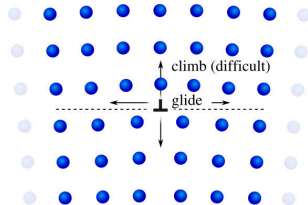


Velocity wrt the applied shear stress  
Adapted from

P. Haasen. *Physical Metallurgy*, Cambridge University Press (1996)

# Dislocation motion II

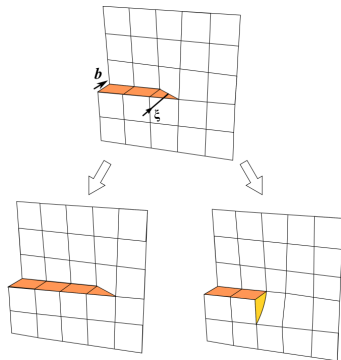
- Note that the Peach-Koehler force is not necessarily in the slip plane  
 $f_{PK} \cdot n \neq 0$
- Glide vs climb
- For edge dislocations:  
**glide** conserves the number of atoms,  
**climb** requires removing or adding lines of atoms (via, e.g. vacancies)
- Edge dislocations rather glide than climb at low temperature
- Very anisotropic motion
- Screw dislocation does not stick to a unique glide plane as  $b \parallel \xi$
- Change of plane by screw dislocations results in **cross-slip**



Climb of screw dislocations requires addition or removal of atoms

# Dislocation motion II

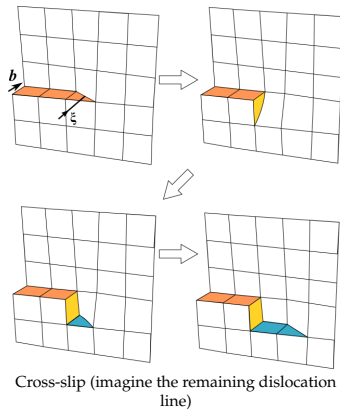
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Screw dislocation may change the plane

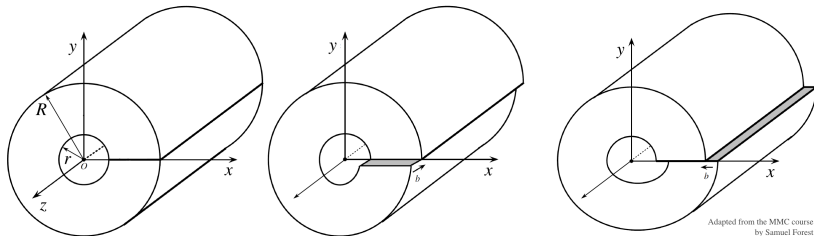
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# Dislocation-induced stress field

## ■ Volterra dislocation<sup>[1]</sup>



## ■ Screw dislocation

$$\sigma_{xz} = -\frac{\mu b}{2\pi} \frac{y}{(x^2 + y^2)}$$

$$\sigma_{yz} = \frac{\mu b}{2\pi} \frac{x}{(x^2 + y^2)}$$

## ■ Edge dislocation

$$\sigma_{xx} = -\frac{\mu b}{2\pi(1-\nu)} \frac{y(3x^2 + y^2)}{(x^2 + y^2)^2}$$

$$\sigma_{yy} = \frac{\mu b}{2\pi(1-\nu)} \frac{y(x^2 - y^2)}{(x^2 + y^2)^2}$$

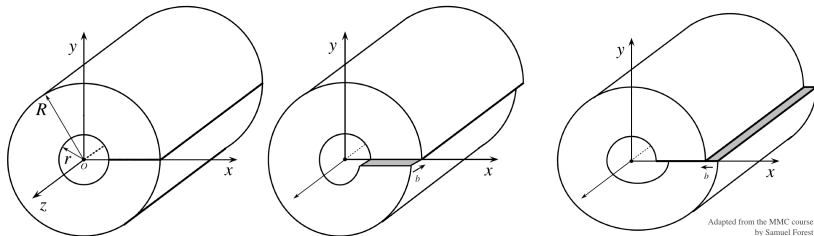
$$\sigma_{xy} = \frac{\mu b}{2\pi(1-\nu)} \frac{x(x^2 - y^2)}{(x^2 + y^2)^2}$$

$$\sigma_{zz} = \nu(\sigma_{xx} + \sigma_{yy})$$

[1] Volterra V. Sur l'équilibre des corps élastiques multiplement connexes. *Annal. Sci. de l'Ecole Norm. Supér.* 24 (1907).

# Dislocation-induced stress field

## ■ Volterra dislocation<sup>[1]</sup>



## ■ Elastic energy per unit length for an edge and screw dislocation

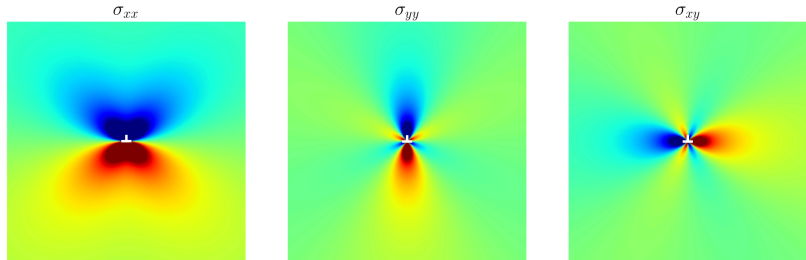
$$E_e = \frac{\mu b^2}{4\pi(1-\nu)} \ln(R/r), \quad E_s = \frac{\mu b^2}{4\pi} \ln(R/r)$$

## ■ For a mixed dislocation (edge $b \sin(\theta)$ , screw $b \cos(\theta)$ )

$$E(\theta) = \frac{\mu b^2(1-\nu \cos^2(\theta))}{4\pi(1-\nu)} \ln(R/r) \approx \alpha \mu b^2, \quad \alpha \approx 0.5 - 1$$

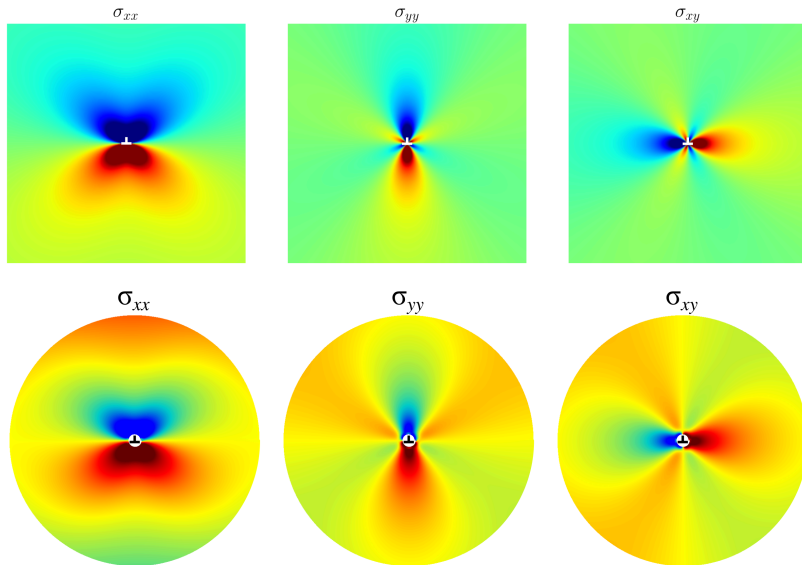
[1] Volterra V. Sur l'équilibre des corps élastiques multiplement connexes. Annal. Sci. de l'Ecole Norm. Supér. 24 (1907).

# Dislocation-induced stress field



Theoretical stress field

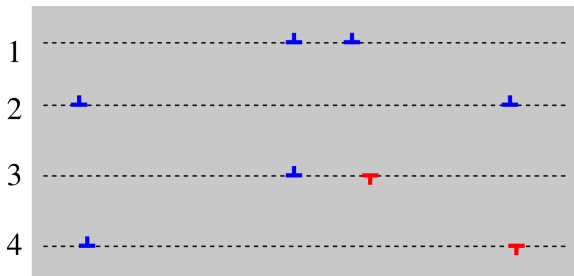
# Dislocation-induced stress field



Comparison with the finite element solution

# Interaction between dislocations

- Interaction between two edge **dislocations on the same line**
- Dislocations of the same sign **repeal** because:
  - when close  $E \approx \mu(2b)^2$
  - when far  $E \approx 2\mu(b)^2$
- Dislocations of opposite sign **attract** because:
  - when close  $E \approx \mu(b - b)^2 = 0$
  - when far  $E \approx 2\mu(b)^2$



# Interaction between dislocations

- Interaction between two edge **dislocations on parallel lines**
- Interaction energy is the work done by the stress field induced by 1 on displacing 2:

$$E_{\text{inter}} = \int_x^{\infty} (\sigma_{xy}b_x + \sigma_{yy}b_y + \sigma_{yz}b_z)dx = - \int_y^{\infty} (\sigma_{xx}b_x + \sigma_{xy}b_y + \sigma_{xz}b_z)dy$$

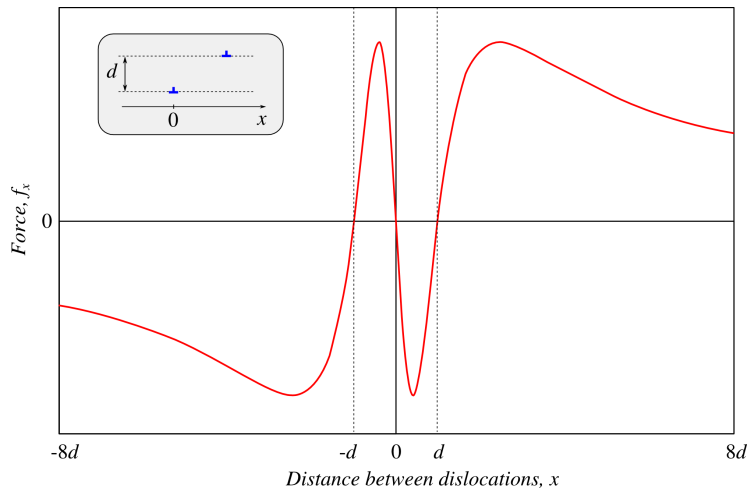
- The resulting forces for two parallel dislocation of the same sign  
 $b_x^1 = b_x^2 = b$ :

$$f_x = -\frac{\partial E_{\text{inter}}}{\partial x} = \frac{\mu b^2}{2\pi(1-\nu)} \frac{x(x^2 - y^2)}{(x^2 + y^2)^2}$$

$$f_y = -\frac{\partial E_{\text{inter}}}{\partial y} = \frac{\mu b^2}{2\pi(1-\nu)} \frac{y(3x^2 - y^2)}{(x^2 + y^2)^2}$$

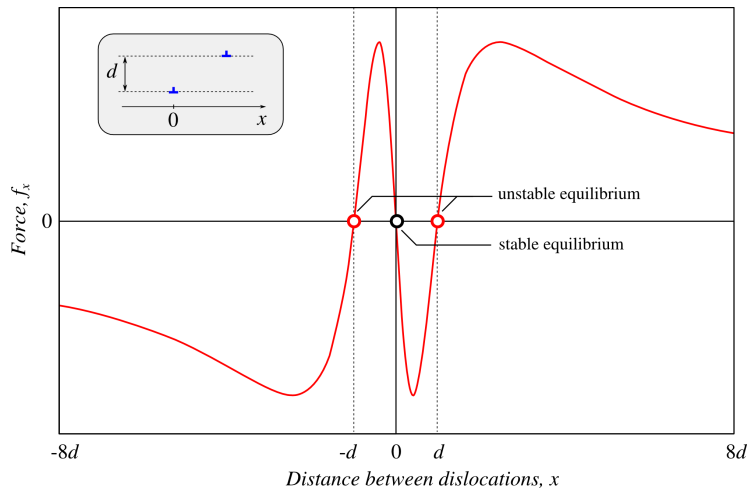
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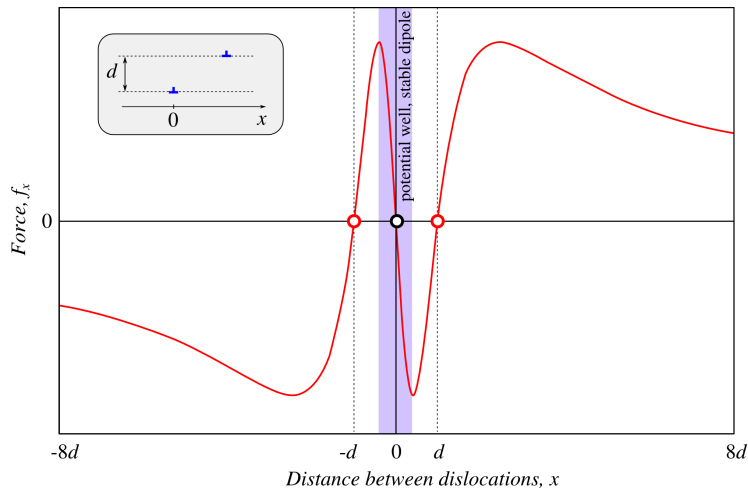
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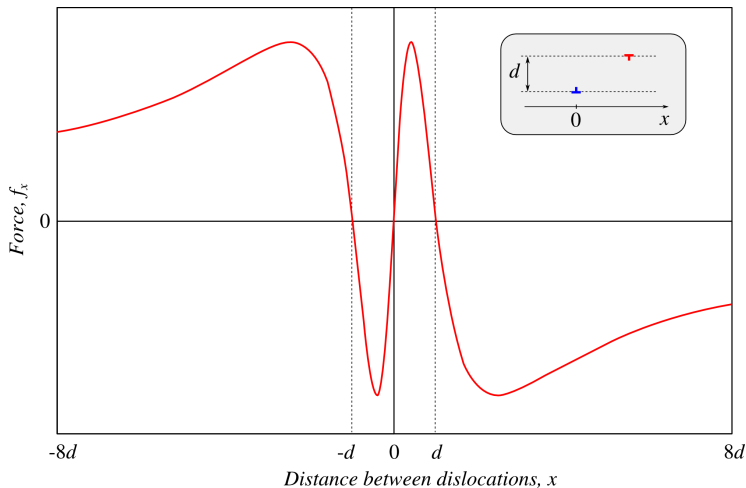
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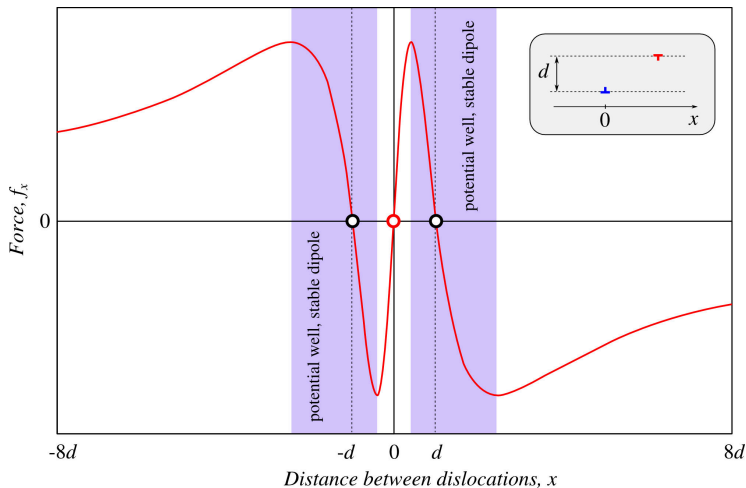
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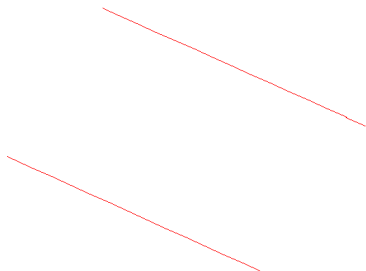
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# Interaction between dislocations

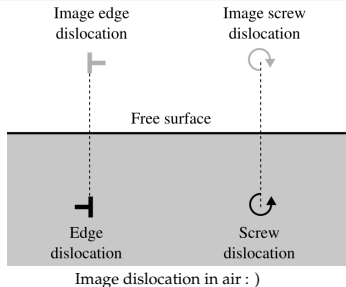
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*from Marc Fivel (SiMap, INP Grenoble), [www.numodis.fr/tridis](http://www.numodis.fr/tridis)*

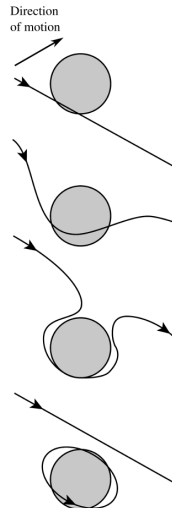
# Dislocations interact with the environment

- **Free surface**  $\sigma \cdot n = 0$
- To ensure zero stress vector, introduce an “image dislocation” of the opposite sign at the same distance from the surface:
$$(\sigma^{\text{real}} + \sigma^{\text{imag}}) \cdot n = 0$$
- Dislocations of opposite sign on the same line **attract each other**
- Note: an additional energy is needed to brake the oxide film
- **Rigid wall**  $u = 0$ , repulsion
- **Rigid inclusions** do not let dislocations glide quietly



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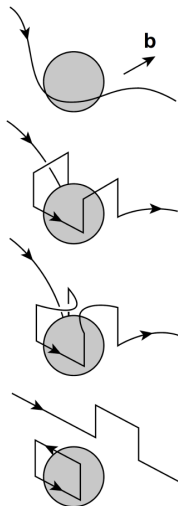
Interaction with a particle in dispersion-strengthened alloy

## Orowan mechanism

Hirsch P.B., Humphreys F.J. Physics of Strength and Plasticity, Ed. A.S. Argon, MIT Press (1969)

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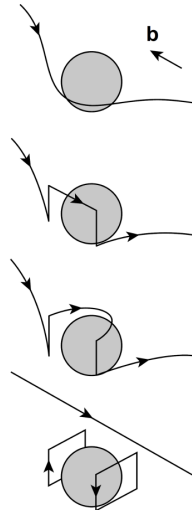
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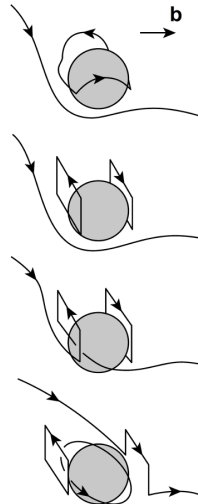
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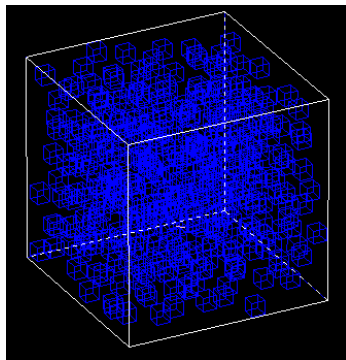
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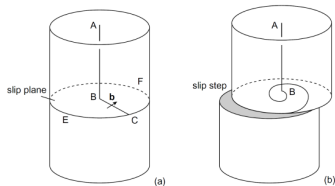
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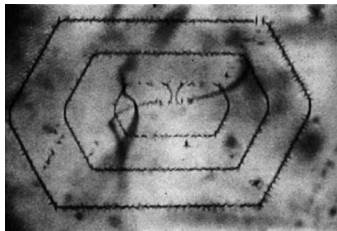
*from Marc Fivel (SiMap, INP Grenoble),  
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# Origin of dislocations

- In virgin well-annealed crystal  
 $\rho \approx 10^{10} \text{ m}^{-2}$
- At early stages of deformation: single set of parallel slip planes is active
- At large deformation:  $\rho \approx 10^{15} \text{ m}^{-2}$ , different slip systems are activated
- At lattice defects and due to stress concentrators
- At grain boundaries
- Frank-Read sources (double and single ended)
- From the free surface
- Geometrically necessary dislocations to accommodate indenter's form



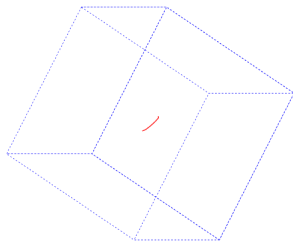
Single-ended Frank-Read source  
from D. Hull, D.J. Bacon, *Introduction to Dislocations*, Elsevier (2011)



Double-ended Frank-Read source in silicon crystal  
from Dash, *Dislocation and Mechanical Properties of Crystals*, Wiley (1957)

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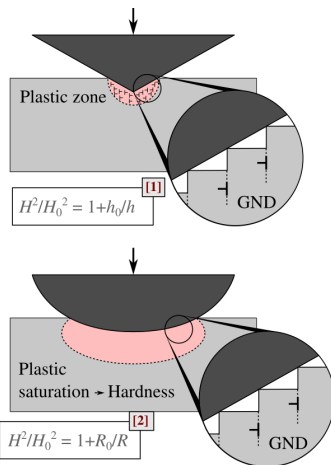
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DD simulation of double ended Frank-Read  
source in a cube-shaped box with rigid walls

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Size effect in nano-indentation due to geometrically necessary dislocations

- [1] Nix, Gao. J Mech Phys Solids (1998)  
[2] Swadener, George, Pharr. J Mech Phys Solids (2002)

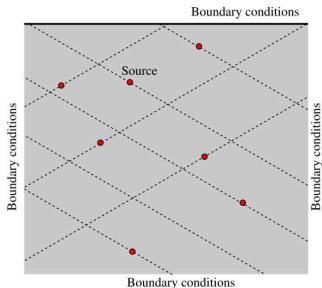
# Simulation of dislocations in 2D

## 2D DD<sup>[1]</sup>

- Infinite straight and parallel dislocations
- No line tension
- No topological changes and intersections

### Ingredients

- Only edge dislocations (points) randomly distributed on discrete slip lines
- Randomly distributed sources with stress and distance threshold:  
 $|f| > f_{nuc}$  : generates  $\pm b$  dislocations at distance:  $l_n = \mu b / [2\pi(1 - \nu)f_{nuc}]$
- On slip lines, randomly distributed obstacles with strength  $f_{obs}^i$



R. Van der Giessen, A. Needleman. Discrete dislocation plasticity: a simple planar model. Model Sim Mater Sci Eng (1995)

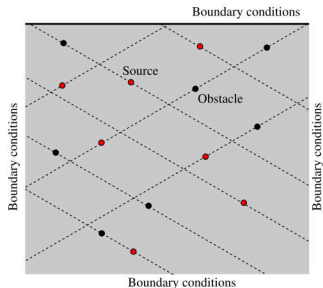
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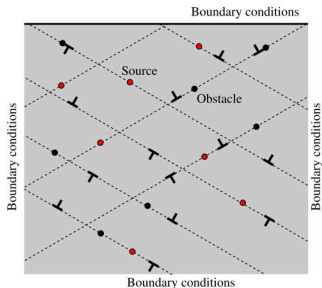
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# Simulation of dislocations in 2D

## Algorithm

- Impose an external stress field  $\sigma^{ext}(x, y)$
- Find Peach-Koehler force on each source from external stress  $f_i^{ext}$  and from dislocations  $f_i^d$

- If  $|f_i^{ext} + f_i^d| \geq f_{nuc}$ : create  $\pm b$  dislocations

- Compute forces on all dislocations

$$f_j = - \sum \nabla_x E_{int}(x_i, x_j) + f_i^{ext}$$

- Assume linear relation between velocity and PK force:

$$f_j = B\dot{x}_j$$

- Integrate in time *Euler-trapezoid method*:

$$x_j^E(t + \Delta t) = x_j(t) + \frac{1}{B} f_j(x(t))$$

$$x_j(t + \Delta t) = x_j(t) + \frac{1}{2B} \left[ f_j(x(t)) + f_j(x^E(t + \Delta t)) \right]$$

# Simulation of dislocations in 2D

## Algorithm

- Impose an external stress field  $\sigma^{ext}(x, y)$
- Find Peach-Koehler force on each source from external stress  $f_i^{ext}$  and from dislocations  $f_i^d$

- If  $|f_i^{ext} + f_i^d| \geq f_{nuc}$ : create  $\pm b$  dislocations

- Compute forces on all dislocations

$$f_j = - \sum \nabla_x E_{int}(x_i, x_j) + f_i^{ext}$$

- Assume linear relation between velocity and PK force:

$$f_j = B\dot{x}_j$$

- Integrate in time *Euler-trapezoid method*:

$$x_j^E(t + \Delta t) = x_j(t) + \frac{1}{B} f_j(x(t))$$

$$x_j(t + \Delta t) = x_j(t) + \frac{1}{2B} \left[ f_j(x(t)) + f_j(x^E(t + \Delta t)) \right]$$

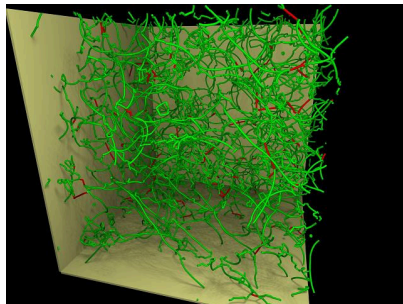
# Simulation of dislocations in 3D

## 3D DD<sup>[1]</sup>

- Splines or edge/screw segments
- Glide and climb
- Arbitrary morphology of dislocations
- Topological changes and intersections
- Enhanced interaction with the material and boundaries

## Ingredients

- Frank-Read sources
- Free-surface
- Grain boundaries
- Possible coupling with the FEM method and with MD both in 2D and 3D



# Simulation of dislocations in 3D

## Algorithm

- Impose/compute via FEM a stress field  $\sigma^{ext}(x, y)$
- Use shape functions for positions and velocities:

$$\mathbf{r}(\xi, t) = N_i(\xi)\mathbf{r}_i(t) \quad \mathbf{v}(\xi, t) = N_i(\xi)\mathbf{v}_i(t)$$

- Find Peach-Koehler force on each node from external stress  $f_i^{ext}$  and from all dislocation segments  $f_i^d = - \int_{D^j} \nabla_x E_{inter} d\Gamma$
- Assume over-damped dynamics, drag force is a linear (in simplest case) function of velocity:

$$\mathbf{f}_j^{drag} = -\mathbf{B} \cdot \mathbf{v}_j$$

- Drag force cannot oppose everywhere the PK force, so it is satisfied in a weak sense:

$$\int_D N_i(-\mathbf{B} \cdot \mathbf{v}_j N_j + f^{PK}) dl = 0$$

- Giving the linear system of equations:

$$\sum B_{ij} \cdot \mathbf{v}_j = \mathbf{f}_i, \quad B_{ij} = \int_D -\mathbf{B} N_i N_j dl$$

- Integrate in time *Euler-trapezoid method*:

$$\mathbf{x}_j^E(t + \Delta t) = \mathbf{x}_j(t) + \mathbf{v}_j(t)\Delta t$$

$$\mathbf{x}_j(t + \Delta t) = \mathbf{x}_j(t) + \frac{1}{2}(\mathbf{v}_j(t) + \mathbf{v}_j^E(t + \Delta t))\Delta t$$

## Animations

[www.numodis.fr/](http://www.numodis.fr/)

[optidis.gforge.inria.fr/videos/video.html](http://optidis.gforge.inria.fr/videos/video.html)

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Merci de votre attention !